Optoelectronic performance of AgNW transparent conductive films with different width-to-height ratios and a figure of merit embodying an optical haze

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Optoelectronic performance of AgNW transparent conductive films with different width-to-height ratios and a figure of merit embodying an optical haze



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ABSTRACT

Transparent conductive films (TCFs) based on rectangularly shaped silver nanowires (AgNWs) with different width-to-height ratios were theoretically studied. We show that tall AgNWs (height > width) possess higher transmittance and lower sheet resistance compared to other configurations of AgNWs. Moreover, tall AgNWs possesses significantly higher optical haze, which makes them a transparent conductor of choice for thin solar cell applications. For applications requiring low haze such as displays and touch screens, we propose an updated figure of merit embodying transmittance, sheet resistance and haze, allowing tuning width-to-height ratio to achieve a reasonable AgNW TCF performance trade-off. Obtained results offer a means for deeper analysis of AgNW properties for many optoelectronic applications.

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I. INTRODUCTION

Transparent conductive films (TCFs) are a key component of many optoelectronic devices such as displays, solar cells, touchscreens, and light-emitting diodes.^{1–8} Till date, indium tin oxide (ITO) based TCFs dominate an electronics industry.⁹ But a high fabrication cost and inflexibility of the ITO prevent its application in future generation devices.^{10–14} Among potential candidates (graphene, polymers, zinc oxide and other) to replace the ITO, silver nanowires (AgNWs) offer beneficial transmittance, sheet resistance, fabrication cost, flexibility and stretchability.^{15–22} Two main categories of AgNWs based on fabrication method are chemically synthesized NWs, randomly arranged on the substrate,^{23,24} and uniform NW meshes made by various lithographical approaches.^{25,26} Previous studies showed that the variation of AgNW thickness and surface coverage allow tuning not only the transmittance and sheet resistance, but also the ratio of scattered to total transmitted light – so-called optical haze.^{27–29} Previous studies characterized the optical haze for AgNWs with square and circular cross-section, which thickness ranged from tens to hundreds of nanometers. For instance, AgNW TCFs with diameter below 50 nm possess low haze $\sim 2\%$, vital to obtain displays with crystal-clear image.³⁰ Thicker AgNWs significantly increase the optical haze and improve an absorbance of thin film solar cells due to longer light pathway.³¹

Here we study other AgNW dimensions to deeper understand its influence on the transmittance, sheet resistance and haze. We investigate the rectangularly shaped AgNWs with various width-toheight ratio and demonstrate how these parameters affect AgNW performance. In addition, we update Haacke's figure of merit to enclose the optical haze, which offers a new glance on AgNW performance trade-off.

II. METHODOLOGY

We address the term *flat* AgNW films to the NWs with width exceeding the height or w > h, and the *tall* AgNW films to the NWs with height exceeding the width or w < h. Even though some

of the structures discussed below are difficult to implement today, they possess interest for the next generation of optoelectronic applications. Figures 1 a) and b) shows the geometrical models for flat and tall AgNW films on glass substrate, respectively. Rectangularly shaped AgNWs were uniformly arranged across the substrate with the lattice constant a, height h, and width w. We range h and w from 30 to 500 nm and NW surface coverage SC from 5 to 50% to investigate AgNW performance in the nano- and microscale regions.

A commercial-grade simulator based on the finite-difference time-domain (FDTD) method was used to perform the optical calculations.³² The material index of refraction and extinction coefficient was taken from Ref. 33. The incident light in the visible wavelength range from 400 to 700 nm was illuminated along Z axis. The periodic boundary conditions and perfectly matched layers were applied perpendicular and parallel to Z axis, respectively, and the simulation unit cell was set to a^2 .





FIG. 2. The average transmittance of AgNW films for the NW width w and height h in the range from 30 to 500 nm, and a) 5%, b) 15%, c) 25%, and d) 50% surface coverage SC. The dashed line indicates the AgNWs with w = h. Regions T_{max} and T_{min} show the areas of highest and lowest transmittance, respectively.

| TAB | LE I. | The | aperture | width | tor | various | w/h | and | SC. | Aperture | width | = | a – |
|-----|-------|--------------|------------------|-------|-----|---------|-----|-----|-----|----------|-------|---|-----|
| w = | w×(1- | $+\sqrt{1-}$ | <u>-sc)</u> – w. | | | | | | | | | | |

| w (nm) sc (%) | 40 | 80 ^c | 250 | 500 |
|---------------|--------|-----------------|--------|---------|
| 5 | 1539.7 | 3079.5 | 9623.4 | 19246.8 |
| 15 | 472.5 | 945 | 2953.3 | 5906.5 |
| 25 | 258.6 | 517.1 | 1616 | 3232.1 |
| 50 | 96.6 | 193.1 | 603.6 | 1207.1 |

Optical haze was evaluated as follows:

$$H = \frac{T_S}{T_T} \tag{1}$$

where T_S is the light scattered from AgNWs into the substrate and T_T is the total light transmitted into the substrate through AgNW film. The forward scattered light was calculated using a totalfield scattered-field source, which allows separating the computation region to collect only the scattered field.³⁴

Sheet resistance was calculated by percolation model according to Refs. 35 and 36:

$$R_{sh} = \frac{1}{h\sigma_0 (\phi_f - \phi_{crit})^t},\tag{2}$$

where σ_0 is the conductivity of metal, ϕ_f is the volume fraction of patterned metal film, ϕ_{crit} is the volume fraction threshold when the patterned film changes from insulator to conductor, *h* is the thickness of the patterned metal film and *t* is the critical exponent.

The above-mentioned models were proved to be in good agreement with experimental data and successfully applied by our group in previous works.^{37–40}

III. RESULTS AND DISCUSSION

Figure 2 plots the average transmittance of AgNW films with *w* and *h* each ranging from 30 to 500 nm, and with 5, 15, 25, and 50%

SC. The dashed line indicates the transmittance of AgNWs with a square cross section (w = h). NWs with w = h = 30 nm reach the maximum transmittance of 95% at SC = 5%, and possess ~ 4, 13, 19 and 25.5% higher transmittance than NWs with w = h = 500 nm for 5, 15, 25, and 50% SC respectively. The transmittance above and below dashed line behaves non-mirror-like: the flat NWs retain higher T. Flat NWs with SC = 5% show 91.5% average transmittance against 91.1% for tall NWs, while for SC = 15, 25, and 50% this difference becomes larger - 80.4 vs 79.2%, 68.9 vs 65.4%, and 46.3 vs 31.3%. The AgNWs with $w = h \le 100$ nm (region T_{max} in Fig. 2) exhibit high transmittance due to stronger coupling of the incoming light to surface plasmons at nanoscale dimensions with maximum effect when h is close to metal skin depth (~ 15-50 nm for the Ag/air interface in the visible range).^{41–44} The AgNWs with $w \le 40$ nm, SC = 25%and $w \le 80$ nm, SC = 50% possess low transmittance for h > 100 nm (region T_{min} in Fig. 2) due to the subwavelength aperture width a – w, which is less than 260 nm (see Table I).

Figures 3a and 3b demonstrates the average transmittance and sheet resistance of AgNW films against the ratio of NW width-toheight w/h with the fixed NW cross section area $w \times h = 15$ k nm². The transmittance increases with higher w/h ratio – 92, 85, 76, and 57% for w/h = 500/30 vs 90, 74, 40 and 1% for w/h = 30/500 at 5, 15, 25, and 50% SC respectively. The sheet resistance also increases, but by ~ 16.7 times - from few to hundred Ohm/sq, which may significantly affect AgNW performance. This happens due to the decrease of the NW height from 500 to 30 nm (see Eq. 2). To understand how w/h ratio affects both AgNW transmittance and sheet resistance Fig. 3c plots AgNW performance for w/h = 500/30, 250/60, 122.5/122.5, 60/250 and 30/500. AgNW performance increases when w/h ratio lowers, which results in the decrease of the sheet resistance. For example, AgNWs with w/h = 500/30 and 30/500 possess 90% transmittance at 90 and 12 Ohm/sq sheet resistance respectively (see the vertical dashed line in Fig. 3c). Thus, we can claim that tall AgNWs outperform not only flat ones, but even AgNWs with square and circular cross sections. Also, tall AgNWs possess smaller lattice constant useful for some optoelectronics application sensitive to an electron mean free path.⁴

Figure 4 plots the average haze of AgNW films where *w* and *h* range from 30 to 500 nm, and for 5, 15, 25, and 50% *SC*. NWs with



FIG. 3. a) The average transmittance and b) sheet resistance of AgNW films against the ratio of NW width-to-height ratio w/h for surface coverage SC = 5, 15, 25, 50% and the fixed NW cross section area $w \times h$ = 15k nm². c) The average transmittance of AgNW films against the sheet resistance for the NW width-to-height ratio w/h = 500/30, 250/60, 122.5/122.5, 60/250, and 30/500.





w = h = 30 nm reach the minimum haze of 1% at SC = 5%, and possess ~ 6.5, 8.5, 15 and 38% lower haze than NWs with w = h =500 nm for 5, 15, 25, and 50% *SC* respectively. Haze above and below dashed line behaves non-mirror-like: the flat NWs retain lower H. Flat NWs with SC = 5% show 6.5% average haze against 10.3% for tall NWs, while for SC = 15, 25, and 50% this difference becomes larger – 8.5 vs 13.3%, 15.5 vs 23.5%, and 42.5 vs 61.8%. AgNWs with $w = h \le$ 100 nm (see region H_{min} on Fig. 4) exhibit lowest haze as a decrease in size of metallic nanostructures reduces the scattering.⁴⁶ When wand h increase, AgNWs start to scatter more light with highest H for h > 100 nm and the subwavelength aperture width (see region H_{max} on Fig. 4).

Figure 5a demonstrates the average haze of AgNW films against the ratio of NW width-to-height w/h with fixed NW cross section area $w \times h = 15$ k nm². The haze increases with lower w/h ratio – 22, 32, 70 and 99% for w/h = 30/500 vs 3.5, 5, 9, and 28% for w/h = 500/30 at 5, 15, 25, and 50% SC respectively. Thus, AgNWs with w/h < 1 definitely suit for thin solar cell applications requiring high H and T, and low R_{sh} . For instance, AgNWs with w/h = 30/500 possess T = 90% at H = 18% and $R_{sh} = 12$ Ohm/sq, while AgNWs with w/h = 500/30 possess same transmittance only at H = 4.5% and R_{sh} = 90 Ohm/sq (see Fig. 5b). In case of application demanding low haze and satisfied by sheet resistance ≥ 100 Ohm/sq (such as touch screens) flat AgNWs are preferable. For other applications requiring



FIG. 5. a) The average haze of AgNW films against the ratio of NW width-to-height *w/h* for 5, 15, 25 and 50% surface coverage *SC* ($w \times h = 15k \text{ nm}^2$). b) The average haze of AgNW films against the sheet resistance for the NW width-to-height ratio *w/h* = 500/30, 250/60, 122.5/122.5, 60/250, and 30/500. Colored dots represent *T* = 90% for the corresponding curves.



FIG. 6. a) Haacke's *FoM*, and b) $FoM_{2\%haze}$ (T_T = 90%, H = 2%) for various AgNW surface coverage SC and width-to-height ratio *w/h*.

low haze and sheet resistance (such as displays), we propose a figure of merit (FoM) enclosing together *T*, *H* and R_{sh} and, hence, allowing to estimate the attractiveness of AgNW TCFs for broad range of applications. In 1972 D.B. Fraser and H.D. Cook first proposed the following equation for FoM of the TCFs:⁴⁷

$$FoM = \frac{T}{R_{sh}}$$
(3)

Several years later G. Haacke showed that the maximum *FoM* in Eq. 3 corresponds to T = 37%, which is not satisfactory for most optoelectronic applications.⁴⁸ G. Haacke modified the Eq. 3 as follows:

$$FoM = \frac{T^{*}}{R_{sh}}$$
(4)

where he set *x* equal to 10 in order to fit the maximum *FoM* for *T* = 90%. Noteworthy, such modification is accurate only for the case when $R_{sh} \ge 1$ Ohm/sq: for example, *T* = 90% and $R_{sh} = 5$ Ohm/sq results in two times lower *FoM* – 0.0697 sq/Ohm, than *T* = 65% and $R_{sh} = 0.1$ Ohm/sq – 0.1346 sq/Ohm.

Here we propose a further update of the Eq. 4 considering the optical haze:

$$FoM = \frac{T_F^x}{R_{sh}}$$
(5)

where T_F is the forward transmitted light into substrate through AgNWs and equals to:

$$T_F = T_T - T_S = T_T (1 - H)$$
(6)

The total transmittance is given by $T_T = \exp(-\alpha h)$, where α is the optical absorption coefficient and h is the thickness of TCF. The value (1 - H) corresponds to the reduction in the total transmittance due to the haze and can be evaluated as $\exp(-\beta h)$, where β is the optical haze-related coefficient. According to above-mentioned expressions, we can rewrite Eq. 5 as follows:

$$FoM = \frac{e^{-hx(\alpha+\beta)}}{R_{sh}}$$
(7)

After deriving Eq. 7 and then equating it to zero, we achieve a maximum value at $h_{max} = [x(\alpha+\beta)]^{-1}$. Substituting h_{max} into $T_F = \exp[-h(\alpha+\beta)]$ we obtain $T_F = \exp(-1/x)$. After merging Eq. 5 and 6 we find expression for *x*:

$$x = -\frac{1}{\ln[T_T(1-H)]} \tag{8}$$

For $T_T = 90\%$ and H = 0 we obtain Haacke's *FoM* with x = 10. For $T_T = 90\%$ and H = 2% x becomes equal to 7.96. Figure 6a plots Haacke's *FoM* for various surface coverage *SC*, where tallest NWs possess the highest performance, which agrees with Fig. 3c. Different behavior is observed for $FoM_{2\%haze}$ (x = 7.96): AgNWs with w/h = 60/250 show up to 1.2 times higher value than AgNWs with other ratios (see Fig. 6b). Indeed, AgNWs with w/h = 60/250 offer attractive T_T , R_{sh} and H parameters: 91.5%, 10 Ohm/sq and 10% respectively (see Table II). For more sensitive display applications AgNWs with w/h = 122.5/122.5 and w/h = 250/60 can be selected as well, possessing lower H (5÷7%) at the cost of higher R_{sh} (21÷45 Ohm/sq). Worth to mention, Haacke's *FoM* matches the situation where high haze of the rectangular shaped AgNWs is demanded.

Figure 7 shows the transmittance, sheet resistance and haze of AgNW films with fixed SC = 5% against the various NW cross section area $w \times h$ and width-to-height ratio w/h. The white solid curve indicates the maximum value of Haacke's *FoM* for each cross-section area appearing at the lowest ratio w/h = 30/500. When NW cross-section area increases from 5k to 25k nm², AgNW transmittance decreases insignificantly – ~1%, while the sheet resistance reduces from 8 to 4 Ohm/sq and haze raises from 13 to 25% resulting in further increase of AgNW performance for thin solar cell applications. The white dashed curve shows the maximum value of $FoM_{2\%haze}$ appearing at ratios $w/h = 0.15 \div 0.35$ retaining *T*, R_{sh} and *H* within 90÷91.5%, 6÷15 Ohm/sq and 15÷8% respectively.

TABLE II. Optical properties of AgNWs with various ratio w/h and SC = 5%.

| Opt. props. <i>w/h</i> | T _T (%) | R _{sh} (Ohm/sq) | H (%) | <i>FoM_{Haacke}</i> (sq/Ohm) | <i>FoM_{2%haze}</i> (sq/Ohm) |
|---------------------------|-----------------------|-----------------------------|----------|---|---|
| 30/500 | 90.9 | 5.3 | 22 | 0.072 | 0.0122 |
| 60/250 | 91.2 | 10.6 | 12 | 0.037 | 0.0162 |
| 122.5/122.5 | 91.8 | 20.1 | 7.5 | 0.021 | 0.0135 |
| 250/60 | 92 | 45 | 5 | 0.01 | 0.0075 |
| 500/30 | 92.5 | 90 | 4 | 0.005 | 0.004 |



FIG. 7. The transmittance, sheet resistance and haze of AgNW films with fixed SC = 5% for the various NW cross-section area $w \times h$ and width-to-height ratio w/h. The white solid and dashed lines indicate the maximum values of Haacke's FoM and FoM_{2%haze} for each cross-section area.

IV. CONCLUSION

TCFs based on rectangularly shaped AgNWs with different width-to-height ratios were theoretically investigated. Tall AgNWs demonstrates higher transmittance and optical haze and lower sheet resistance compared to flat AgNWs makings them a transparent conductive film of choice for thin solar cell applications. We propose an update for Haacke's figure of merit to enclose haze factor, which can be used to find performance trade-off for broader range of applications including those, which require low haze. Obtained results grant an opportunity for deeper analysis of AgNW properties for many optoelectronic applications.

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